



<b>Principal:</b>	CITYFY & BFC Pty Ltd	<b>Job Number:</b>	1806063
<b>Project Title:</b>	Proposed Residential Development	<b>Date:</b>	14 May 2020
<b>Site:</b>	82 Johns Road, Prospect, SA.		

#### ATTACHMENTS:

- SW1 – SW3 - Stormwater Detention Calculations 1:10 Yr ARI, 'Critical Storm' Duration
- SW4 – SW6 - Stormwater Detention Calculations 1:100 Yr ARI, 'Critical Storm' Duration
- BG1 - Box Gutter Calculations 1:100 Yr ARI

#### DESIGN:

The pre development flow off the two allotments is 45.77L/s. 100% of the roof and surface area is to be detained within 13 x 1,500L detention tanks for the units, 8 x 1,000L detention tanks for the dwellings, 10,500L underground tank & 3 above ground basins of 21,333L. Total proposed volume is 59,333L. The OSD is to be discharged at 14.64L/sec into the existing SEP. The 0.9 coefficient is used as only the roof area is being considered for detention.

#### GENERAL NOTES:

1. These calculations are to be read in conjunction with the relevant associated Drawings, Footing Construction Report, Civil Drawings and / or details.
2. All work is to comply with relevant SAA Standards and Guides.

AS 2876-1987: Concrete kerbs and channels (gutters) – manually or machine placed  
 AS 2200-2006: Design charts for water supply and sewerage  
 AS/NZS 3500: Plumbing and drainage  
 AS 3798-1990: Guidelines on earthworks for commercial and residential developments  
 AS 4000-1997:  
     and General conditions of contract  
 AS 2124-1992:  
 ARRB Special Report 35: Subsurface drainage of road structures  
 Australian Rainfall and Run-off Volumes 1 and 2: A guide to flood estimation  
 Austroads 2008 – Guide to pavement technology  
 NAASRA 1987 – Pavement design  
 Storm drainage design in small urban catchments: A handbook for Australian practice  
 Water Sensitive Urban Design (WSUD) Engineering Procedure: Stormwater  
 Water Services Association of Australia Code (WSAA).

For and on behalf of  
**TMK Consulting Engineers**

**Alex Perez**  
 Civil Engineer



Ref.: 1806063

Date: 15-May-20

Design: ALP

Page: SW1

## STORMWATER CALCULATIONS - DETERMINATION OF DETENTION TANK SIZES

Design Storm Intensity Table (mm/hr) - (from <http://www.bom.gov.au/cgi-bin/hydro/has/CDIRSWebBasic>)

### STORM LOCATION

Adelaide

Latitude 34°59'S; Longitude 138°44'E

#### Adelaide

DURATION	AVERAGE RETURN INTERVAL (YEARS)						
	1	2	5	10	20	50	100
5 mins	52.60	69.00	89.40	104.00	123.00	151.00	175.00
6 mins	49.10	64.50	83.50	96.70	115.00	141.00	163.00
10 mins	39.80	52.00	66.90	77.10	91.30	112.00	129.00
20 mins	28.30	36.80	46.80	53.40	62.80	76.20	87.30
30 mins	22.70	29.40	37.10	42.30	49.50	59.80	68.30
1 hour	15.20	19.70	24.60	27.90	32.50	39.00	44.40
2 hours	10.10	13.00	16.20	18.30	21.20	25.40	28.90
3 hours	7.92	10.20	12.70	14.30	16.60	19.90	22.50
6 hours	5.24	6.75	8.37	9.44	11.00	13.10	14.90
12 hours	3.45	4.44	5.52	6.23	7.23	8.65	9.83
24 hours	2.22	2.86	3.58	4.05	4.72	5.66	6.44
48 hours	1.38	1.78	2.24	2.55	2.98	3.60	4.11
72 hours	1.02	1.32	1.67	1.90	2.23	2.70	3.10

### PRE-DEVELOPMENT

Design ARI (yr) 10 yr  
 Design Duration (min) 10 min  
 Design Storm Intensity (mm/hr) 77.10 mm/hr

Design Parameters	C	Area (m <sup>2</sup> )	% Area Detained
Roof	0.90	393	0.00
Paving	0.75	2378	0.00
Grass / Landscaping	0.12	0	0.00
<b>Total Area</b>		<b>2771 m<sup>2</sup></b>	
Weighted C (C <sub>w</sub> )*	0.77		

Max pre-development flow  $Q_i = \Sigma(C_i A_i / 3600)$ :

Roof	7.58 L/s
Paving	38.20 L/s
Grass / Landscaping	0.00 L/s

**Pre-development flow = 45.77 L/s**

**Use Max Allowable Flow = 45.77 L/s**

**Note:** The weighted average value of the runoff coefficient, C<sub>w</sub>, includes roof, paving, grassed and landscaped areas of the site.

### POST-DEVELOPMENT (\*Determine Critical Storm)

Design ARI (yr) 10 yr  
 Design Duration (min) 40 min  
 Design Storm Intensity (mm/hr) 37.50 mm/hr

Design Parameters	C	Area (m <sup>2</sup> )	% Area Detained
Roof	0.90	1329	100.00
Paving	0.75	858	100.00
Grass / Landscaping	0.12	584	0.00
<b>Total Area</b>		<b>2771 m<sup>2</sup></b>	
Weighted C (C <sub>w</sub> )*	0.69		

#### Summary of Design Flows

Undetained flow,  $Q_u = \Sigma(C_u A_u / 3600)$ :

Roof	0.00 L/s
Paving	0.00 L/s
Grass / Landscaping	0.73 L/s

**Design undetained flow = 0.73 L/s**

#### Max. outflows from detention tanks:

Site water runoff	
Pumped	0.00 L/s
Piped	0.00 L/s
Roof water runoff	
Orifice-restricted	12.44 L/s

**Total Max. Design Outflow = 13.17 L/s**

**< 45.77 L/s Allowed ∴ OK**

## STORMWATER CALCULATIONS - STORMWATER RUN-OFF - ORIFICE-RESTRICTED

### Time of Concentration, $T_C$

Design Storm ARI (yr) 10 yr (from page SW1)  
Design Storm Duration (mins) 40 mins (from page SW1)  
Design Storm Intensity,  $i$  37.50 mm/hr (from page SW1)

=> For run-off calculations, use  $T_C =$  **10.0** mins **<=Duration ∴ Use  $T_C = 10$  mins.**

Design Parameters	C	Area (m <sup>2</sup> )	% Area Detained
Roof	0.90	1329	100.00
Paving	0.75	858	100.00
Grass / Landscaping	0.12	584	0.00

Detained flow,  $Q_d = \sum(C_i A_d / 3600)$ :

Roof	12.46 L/s
Paving	6.70 L/s
Grass / Landscaping	0.00 L/s
<b>Design detained flow =</b>	<b>19.16 L/s</b>

### => Try the following retention tank design parameters:

Max Allowable outflow from storage = **14.00** L/s **(31.04 L/s is still available for outflow)**  
Number of orifice detention tanks **1** Each tank volume above orifice **38,000 L**  
Max. head allowed above orifice **1,500** mm => **Each Tank Plan Area =** **25.33 m<sup>2</sup>**  
Outlet coefficient,  $C_o$  **0.6**  
Orifice diameter,  $D_o$  **80** mm => Orifice area,  $A_o = \pi * (D_o / 2)^2$  **5,027 mm<sup>2</sup>**

### Graph Time v Flow:

Time (mins)	InFlow (L/s)	OutFlow (L/s)
0	0.00	0.00
10	19.16	4.85
40	19.16	12.17
50	0.00	11.85

### Max. Calculated Outflow:

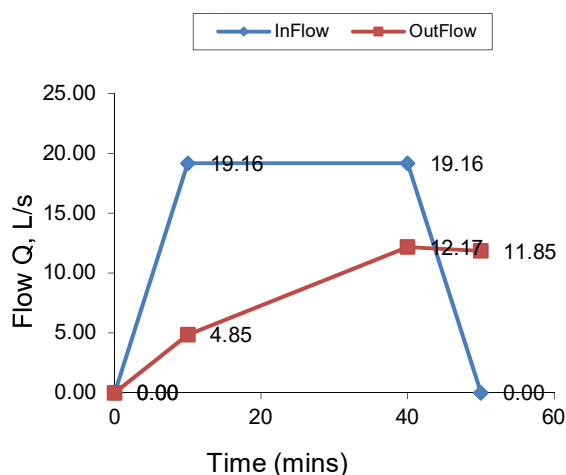
$Q_{max_{out}} =$  **12.44 L/s**

**< 14.00 L/s Max. Allowed ∴ OK**

### Max. Calculated Head of Water:

$H =$  **892 mm**

**< 1,500 mm Max. Allowed ∴ OK**

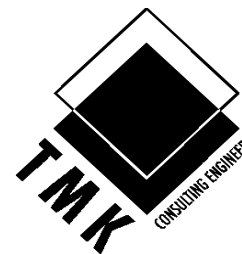


### => Volume of Water To Be Detained:

$V =$  **22,600 L**  
i.e.  $V =$  **22.60 m<sup>3</sup>**

=>USE

Duration (mins)	Intensity (mm/hr)	Proposed Inflow Rate (L/s)	Proposed Inflow Rate x Duration (L)	Orifice Outflow Rate (L/s)	Orifice Outflow Volume (L)	Net Storage (L)
5	104.00	53.1	15,943	-14.00	-2,520	13,423
6	96.70	49.4	17,789	-14.00	-3,024	14,765
7	91.80	46.9	19,702	-14.00	-3,528	16,174
8	86.90	44.4	21,315	-14.00	-4,032	17,283
9	82.00	41.9	22,627	-14.00	-4,536	18,091
10	77.10	39.4	23,639	-14.00	-5,040	18,599
11	74.73	38.2	25,203	-14.00	-5,544	19,659
12	72.36	37.0	26,623	-14.00	-6,048	20,575
13	69.99	35.8	27,897	-14.00	-6,552	21,345
14	67.62	34.6	29,025	-14.00	-7,056	21,969
15	65.25	33.3	30,008	-14.00	-7,560	22,448
16	62.88	32.1	30,846	-14.00	-8,064	22,782
17	60.51	30.9	31,539	-14.00	-8,568	22,971
18	58.14	29.7	32,086	-14.00	-9,072	23,014
19	55.77	28.5	32,488	-14.00	-9,576	22,912
20	53.40	27.3	32,745	-14.00	-10,080	22,665
25	47.85	24.5	36,677	-14.00	-12,600	24,077
30	42.30	21.6	38,908	-14.00	-15,120	23,788
35	39.90	20.4	42,817	-14.00	-17,640	25,177
<b>40</b>	<b>37.50</b>	<b>19.2</b>	<b>45,990</b>	<b>-14.00</b>	<b>-20,160</b>	<b>25,830</b>
45	35.10	17.9	48,427	-14.00	-22,680	25,747
50	32.70	16.7	50,129	-14.00	-25,200	24,929
55	30.30	15.5	51,095	-14.00	-27,720	23,375
60	27.90	14.3	51,325	-14.00	-30,240	21,085
75	25.50	13.0	58,637	-14.00	-37,800	20,837
90	23.10	11.8	63,742	-14.00	-45,360	18,382
120	18.30	9.4	67,329	-14.00	-60,480	6,849
150	16.30	8.3	74,964	-14.00	-75,600	636



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Date: 15-May-20  
Design: ALP  
Page: SW3

### CRITICAL STORM DURATION ORIFICE OUTFLOW

Critical Storm Duration = 40 mins  
Max Storage Volume = 25,830 Litres

**\*Notes:** This calculation is used for determining the critical storm duration at the location shown on the main calculation sheet for the case where the maximum outflow rate from the tank orifice is as shown in the table.

The Net Storage Volume values shown in this table are approximate. The design uses results obtained from calculations where the effects of the change in head in the storage tank and the Time of Concentration have been included.

The critical storm results are shown highlighted in bold italics.



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Date: 15-May-20

Design: ALP

Page: SW4

## STORMWATER CALCULATIONS - DETERMINATION OF DETENTION TANK SIZES

Design Storm Intensity Table (mm/hr) - (from <http://www.bom.gov.au/cgi-bin/hydro/has/CDIRSWebBasic>)

### STORM LOCATION

Adelaide

Latitude 34°59'S; Longitude 138°44'E

#### Adelaide

DURATION	AVERAGE RETURN INTERVAL (YEARS)						
	1	2	5	10	20	50	100
5 mins	52.60	69.00	89.40	104.00	123.00	151.00	175.00
6 mins	49.10	64.50	83.50	96.70	115.00	141.00	163.00
10 mins	39.80	52.00	66.90	77.10	91.30	112.00	129.00
20 mins	28.30	36.80	46.80	53.40	62.80	76.20	87.30
30 mins	22.70	29.40	37.10	42.30	49.50	59.80	68.30
1 hour	15.20	19.70	24.60	27.90	32.50	39.00	44.40
2 hours	10.10	13.00	16.20	18.30	21.20	25.40	28.90
3 hours	7.92	10.20	12.70	14.30	16.60	19.90	22.50
6 hours	5.24	6.75	8.37	9.44	11.00	13.10	14.90
12 hours	3.45	4.44	5.52	6.23	7.23	8.65	9.83
24 hours	2.22	2.86	3.58	4.05	4.72	5.66	6.44
48 hours	1.38	1.78	2.24	2.55	2.98	3.60	4.11
72 hours	1.02	1.32	1.67	1.90	2.23	2.70	3.10

### PRE-DEVELOPMENT

Design ARI (yr) 10 yr  
 Design Duration (min) 10 min  
 Design Storm Intensity (mm/hr) 77.10 mm/hr

Design Parameters	C	Area (m <sup>2</sup> )	% Area Detained
Roof	0.90	393	0.00
Paving	0.75	2378	0.00
Grass / Landscaping	0.12	0	0.00
<b>Total Area</b>		<b>2771 m<sup>2</sup></b>	
Weighted C (C <sub>w</sub> )*	0.77		

Max pre-development flow  $Q_i = \Sigma(C_i A_i / 3600)$ :

Roof	7.58 L/s
Paving	38.20 L/s
Grass / Landscaping	0.00 L/s

**Pre-development flow = 45.77 L/s**

**Use Max Allowable Flow = 45.77 L/s**

**Note:** The weighted average value of the runoff coefficient, C<sub>w</sub>, includes roof, paving, grassed and landscaped areas of the site.

### POST-DEVELOPMENT (\*Determine Critical Storm)

Design ARI (yr) 100 yr  
 Design Duration (min) 90 min  
 Design Storm Intensity (mm/hr) 36.65 mm/hr

Design Parameters	C	Area (m <sup>2</sup> )	% Area Detained
Roof	0.90	1329	100.00
Paving	0.75	858	100.00
Grass / Landscaping	0.12	584	0.00
<b>Total Area</b>		<b>2771 m<sup>2</sup></b>	
Weighted C (C <sub>w</sub> )*	0.69		

#### Summary of Design Flows

Undetained flow,  $Q_u = \Sigma(C_u A_u / 3600)$ :

Roof	0.00 L/s
Paving	0.00 L/s
Grass / Landscaping	0.71 L/s

**Design undetained flow = 0.71 L/s**

#### Max. outflows from detention tanks:

Site water runoff	
Pumped	0.00 L/s
Piped	0.00 L/s
Roof water runoff	
Orifice-restricted	13.92 L/s

**Total Max. Design Outflow = 14.64 L/s**

**< 45.77 L/s Allowed ∴ OK**

## STORMWATER CALCULATIONS - STORMWATER RUN-OFF - ORIFICE-RESTRICTED

### Time of Concentration, $T_C$

Design Storm ARI (yr) 100 yr (from page SW4)  
Design Storm Duration (mins) 90 mins (from page SW4)  
Design Storm Intensity,  $i$  36.65 mm/hr (from page SW4)

=> For run-off calculations, use  $T_C =$  **10.0** mins **<=Duration ∴ Use  $T_C = 10$  mins.**

Design Parameters	C	Area (m <sup>2</sup> )	% Area Detained
Roof	0.90	1329	100.00
Paving	0.75	858	100.00
Grass / Landscaping	0.12	584	0.00

Detained flow,  $Q_d = \sum(CiA_d/3600)$ :

Roof	12.18 L/s
Paving	6.55 L/s
Grass / Landscaping	0.00 L/s
<b>Design detained flow =</b>	<b>18.73 L/s</b>

### => Try the following retention tank design parameters:

Max Allowable outflow from storage = **14.00** L/s **(31.06 L/s is still available for outflow)**

Number of orifice detention tanks **1** Each tank volume above orifice **59,333 L**

Max. head allowed above orifice **1,500** mm => **Each Tank Plan Area =** **39.56 m<sup>2</sup>**

Outlet coefficient,  $C_o$  **0.6**

Orifice diameter,  $D_o$  **80** mm => Orifice area,  $A_o = \pi \cdot (D_o/2)^2$  **5,027 mm<sup>2</sup>**

### Graph Time v Flow:

Time (mins)	InFlow (L/s)	OutFlow (L/s)
0	0.00	0.00
10	18.73	3.68
90	18.73	13.84
100	0.00	13.49

### Max. Calculated Outflow:

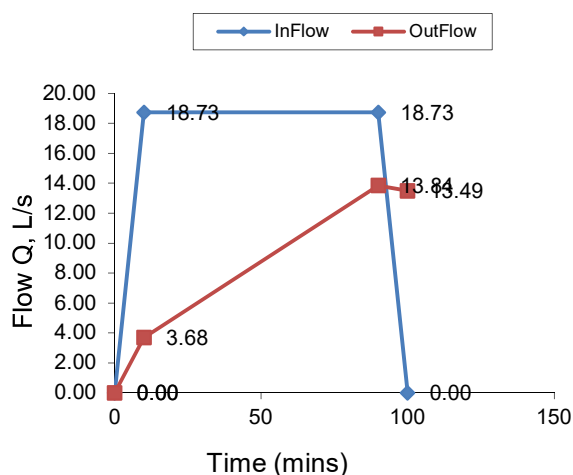
$Q_{max_{out}} =$  **13.92 L/s**

**< 14.00 L/s Max. Allowed ∴ OK**

### Max. Calculated Head of Water:

$H =$  **1,116 mm**

**< 1,500 mm Max. Allowed ∴ OK**

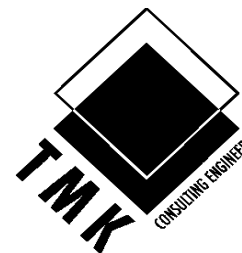


### => Volume of Water To Be Detained:

$V =$  **44,136 L**  
i.e.  $V =$  **44.14 m<sup>3</sup>**

=>USE

Duration (mins)	Intensity (mm/hr)	Proposed Inflow Rate (L/s)	Proposed Inflow Rate x Duration (L)	Orifice Outflow Rate (L/s)	Orifice Outflow Volume (L)	Net Storage (L)
5	175.00	89.4	26,828	-14.00	-2,520	24,308
6	163.00	83.3	29,985	-14.00	-3,024	26,961
7	154.50	78.9	33,159	-14.00	-3,528	29,631
8	146.00	74.6	35,811	-14.00	-4,032	31,779
9	137.50	70.3	37,942	-14.00	-4,536	33,406
10	129.00	65.9	39,551	-14.00	-5,040	34,511
11	124.83	63.8	42,100	-14.00	-5,544	36,556
12	120.66	61.7	44,393	-14.00	-6,048	38,345
13	116.49	59.5	46,431	-14.00	-6,552	39,879
14	112.32	57.4	48,212	-14.00	-7,056	41,156
15	108.15	55.3	49,738	-14.00	-7,560	42,178
16	103.98	53.1	51,008	-14.00	-8,064	42,944
17	99.81	51.0	52,023	-14.00	-8,568	43,455
18	95.64	48.9	52,782	-14.00	-9,072	43,710
19	91.47	46.7	53,285	-14.00	-9,576	43,709
20	87.30	44.6	53,532	-14.00	-10,080	43,452
25	77.80	39.8	59,634	-14.00	-12,600	47,034
30	68.30	34.9	62,822	-14.00	-15,120	47,702
35	64.32	32.9	69,018	-14.00	-17,640	51,378
40	60.33	30.8	73,993	-14.00	-20,160	53,833
45	56.35	28.8	77,746	-14.00	-22,680	55,066
50	52.37	26.8	80,278	-14.00	-25,200	55,078
55	48.38	24.7	81,589	-14.00	-27,720	53,869
60	44.40	22.7	81,678	-14.00	-30,240	51,438
75	40.53	20.7	93,187	-14.00	-37,800	55,387
<b>90</b>	<b>36.65</b>	<b>18.7</b>	<b>101,132</b>	<b>-14.00</b>	<b>-45,360</b>	<b>55,772</b>
120	28.90	14.8	106,329	-14.00	-60,480	45,849
150	25.70	13.1	118,194	-14.00	-75,600	42,594
180	22.50	11.5	124,173	-14.00	-90,720	33,453
210	21.23	10.9	136,713	-14.00	-105,840	30,873
240	19.97	10.2	146,923	-14.00	-120,960	25,963
270	18.70	9.6	154,802	-14.00	-136,080	18,722
300	17.43	8.9	160,352	-14.00	-151,200	9,152
330	16.17	8.3	163,571	-14.00	-166,320	2,749



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Date: 15-May-20  
Design: ALP  
Page: SW6

### CRITICAL STORM DURATION ORIFICE OUTFLOW

Critical Storm Duration = 90 mins  
Max Storage Volume = 55,772 Litres

**\*Notes:** This calculation is used for determining the critical storm duration at the location shown on the main calculation sheet for the case where the maximum outflow rate from the tank orifice is as shown in the table.

The Net Storage Volume values shown in this table are approximate. The design uses results obtained from calculations where the effects of the change in head in the storage tank and the Time of Concentration have been included.

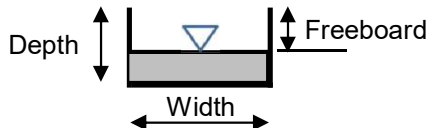
The critical storm results are shown highlighted in bold italics.



Ref.: 1806063  
 Date: 15-May-20  
 Design: ALP  
 Page: BG1

## BOX GUTTER & DOWNPIPE SPECIFICATIONS

### INPUT DATA:



**Gutter Geometry**

Design Storm Event –  $\left\{ \begin{array}{l} \text{ARI} = 100 \text{ years} \\ \text{Duration} = 5 \text{ minutes} \end{array} \right.$

Gutter width = 0.400 metres  
 Gutter depth = 0.100 metres  
 Gutter freeboard = 0.025 metres  
 Box gutter sump depth (below gutter invert) = 0.100 metres  
 Longest gutter run = 4.70 metres  
 Downpipe diameter = 0.150 metres

Cross section area of downpipe,  $A_{\text{pipe}} = 0.0177 \text{ m}^2$   
 Design water section area in box gutter,  $A_{\text{box}} = 0.03 \text{ m}^2$   
 Roughness coefficient,  $n = 0.009$   
 Fittings head loss coefficient,  $k = 2.5$   
 Average gradient,  $s = 0.005$

### DETERMINE FLOWS:

$A_{\text{roof}} = 64 \text{ m}^2$  (The largest roof area contributing runoff into a downpipe/sump)  
 $C = 1.08$  (Runoff coefficient ( $C_{10} \cdot F_y$ ))  
 $I = 175 \text{ mm/hr}$

$Q_{\text{roof}} = CIA_{\text{roof}} / 3600 = 3.36 \text{ L/Sec}$   
 $Q_{\text{box}} = A_{\text{box}} R^{2/3} S^{1/2} / n = 33.90 \text{ L/Sec} \quad \therefore \text{OK. } Q_{\text{box}} > Q_{\text{roof}}$   
 where  $R = A_{\text{box}} / P_{\text{box (wetted perimeter)}} = 0.05 \text{ metres}$

### CHECK ENTRY INTO DOWNPIPE AND WATER LEVEL BUILD-UP:

$V = (Q_{\text{roof}} / A_{\text{pipe}}) / 1000 = 0.190 \text{ m/s}$

Velocity head required  $= kV^2/2g = 0.005 \text{ m}$   
 Depth required due to length of gutter fall = 0.024 m  
 Adopted freeboard = 0.025 m  
**Total gutter & sump depth required = 0.053 m**  
**Selected gutter & sump depth = 0.200 m**  
 **$\therefore$  Box Gutter size is OK**

### ADOPT:

0.400 m wide x 0.100 m Deep Box Gutter  
 0.150 m Diameter Downpipes  
 0.100 m Deep Box Gutter Sumps